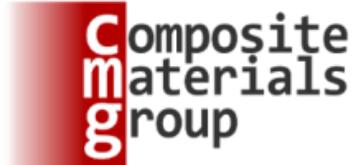


Experimental challenges in DCB testing of thin composite laminates

Panayiotis Tsokanas
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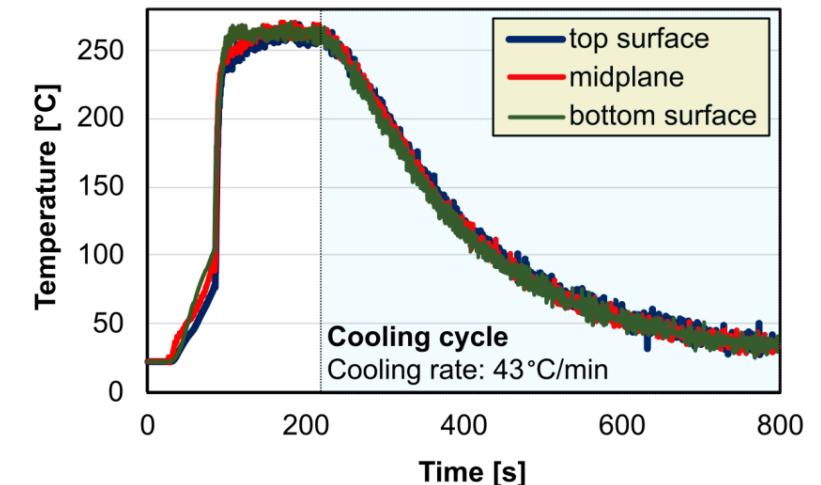
Online Workshop ‘Mode I interlaminar fracture
toughness and the factors affecting it’
14 May 2024



Thin composite laminates

Need for thin laminates

- Material savings
- Manufacturing thermal history that can be assumed isothermal through the thickness, which is essential for semi-crystalline polymers, whose material crystallinity is crucial in mechanical and interlaminar properties.

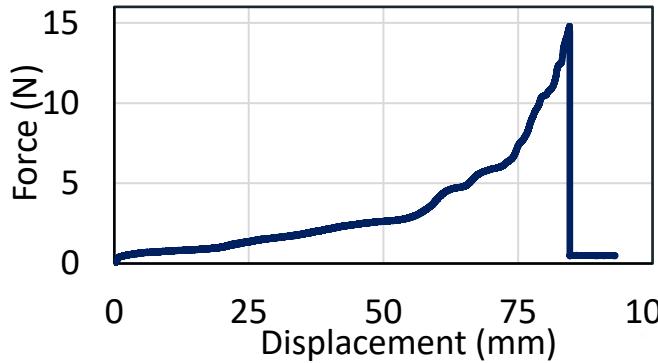


Reasons to test thin laminates (and not following the ASTM thickness)

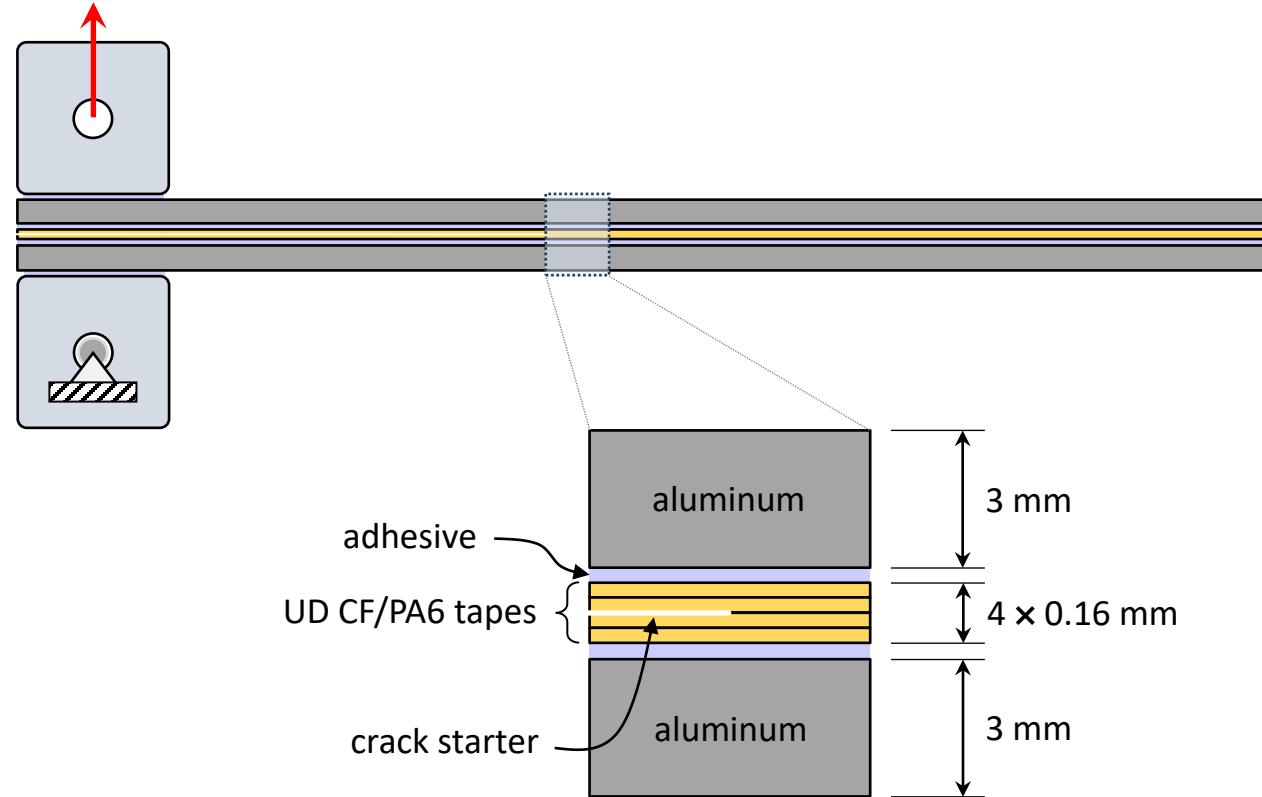
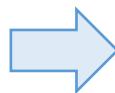
- Make sure about uniform cooling rate across the thickness
- Representativeness for those applications where thin laminates are needed



Material yielding or sudden breakage

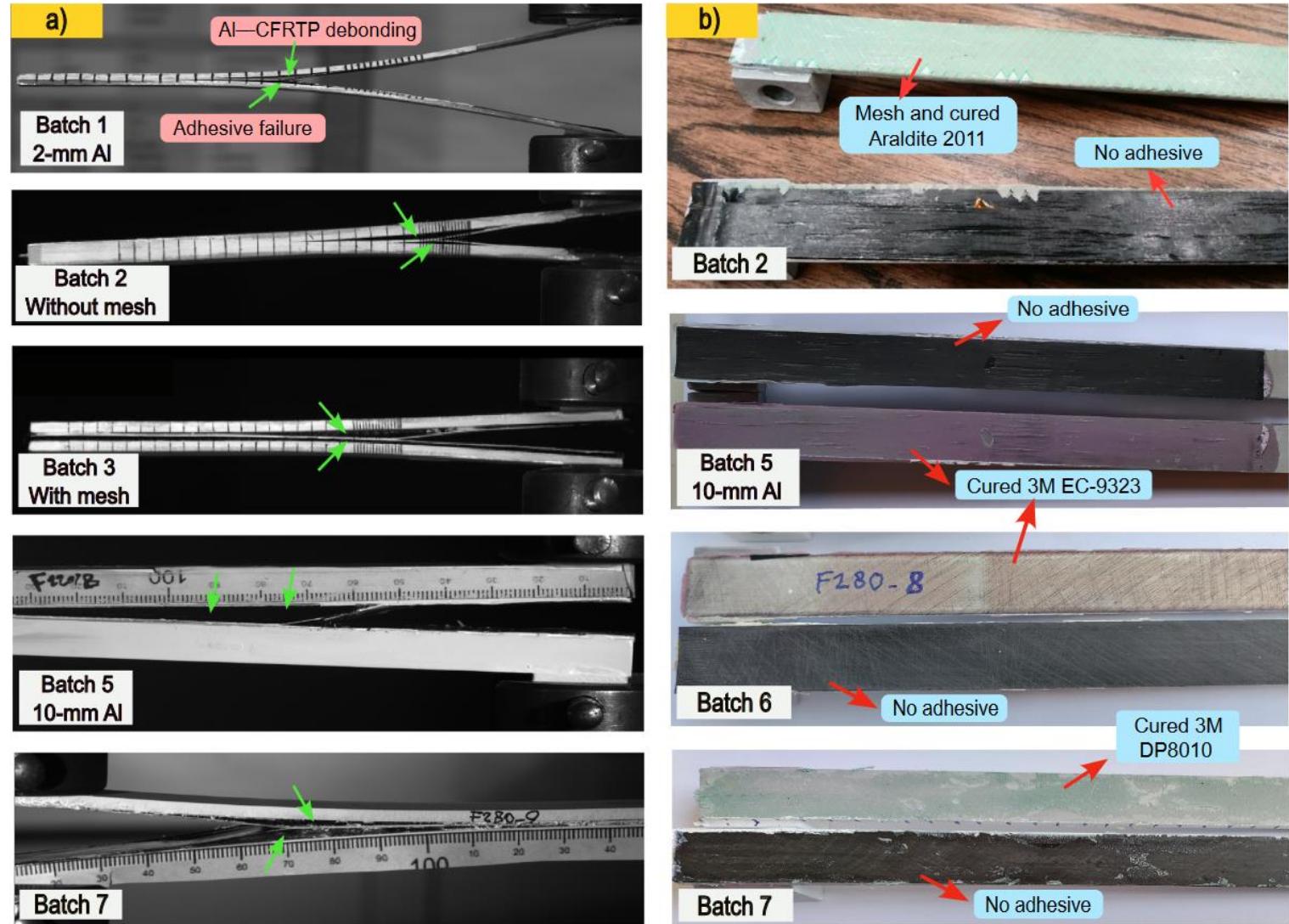


80 mm extension, no crack initiation →
sudden arm break occurred

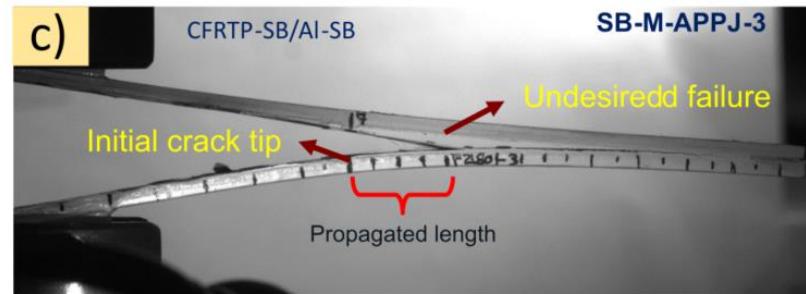
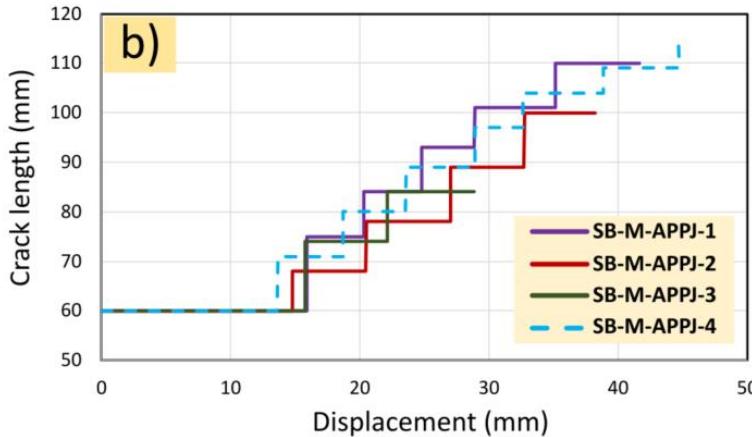
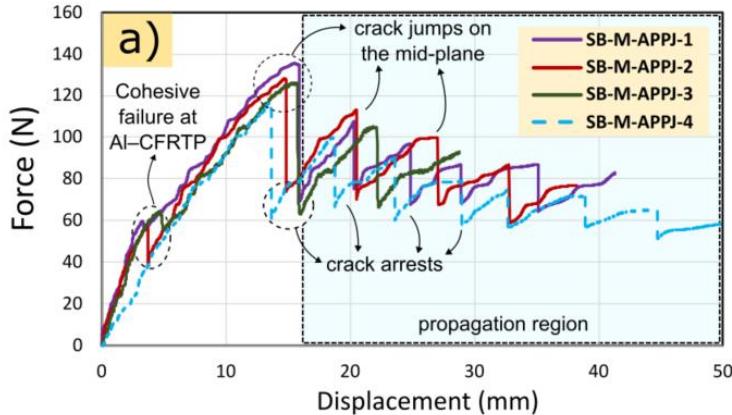


Adhesion issues to the stiffeners

- Low surface energy and wettability issues
- CF/PA6 thermoplastic fracture toughness is higher than most of the (thermoset-based) adhesives, and crack initiation at the Al–CFRTP interface is inevitable

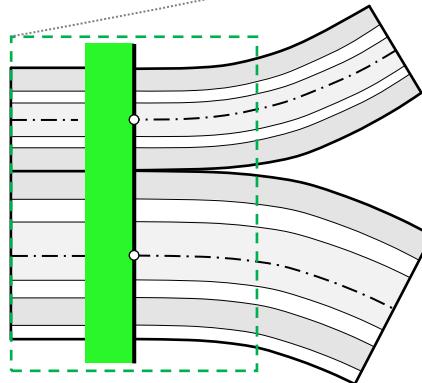
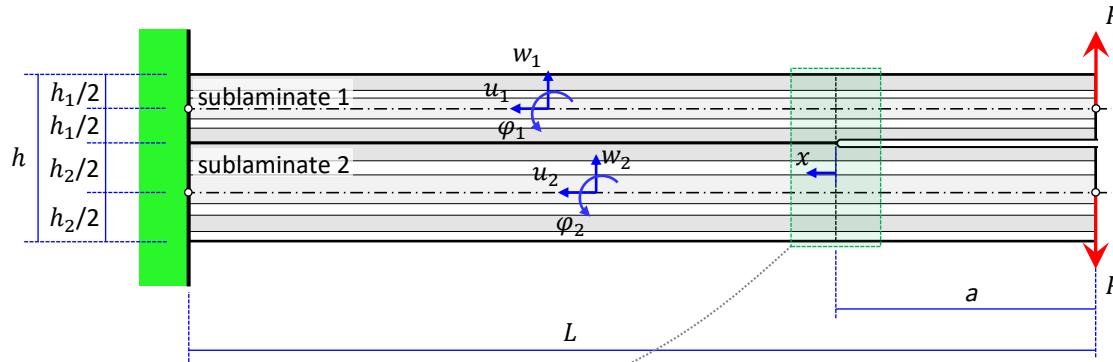


Atmospheric pressure plasma jet (APPJ) treatment



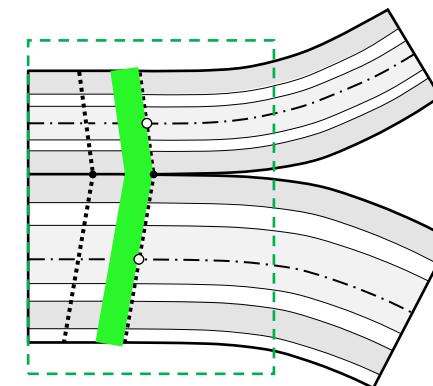
The composite interface is tougher than the adhesive

Experimental data reduction



Clamped model

(Valvo, 2016)



Semi-rigid model

(Tsokanas & Loutas, 2019;
Tsokanas & Loutas, 2022)

Clamped model (Valvo, 2016)

$$G_I = \frac{P^2}{2} \left\{ \left[d_1 + d_2 - \frac{\left(b_1 + b_2 + d_1 \frac{h_1}{2} - d_2 \frac{h_2}{2} \right)^2}{a_1 + a_2 + b_1 h_1 - b_2 h_2 + d_1 \frac{h_1^2}{4} + d_2 \frac{h_2^2}{4}} \right] a^2 + c_1 + c_2 \right\}$$

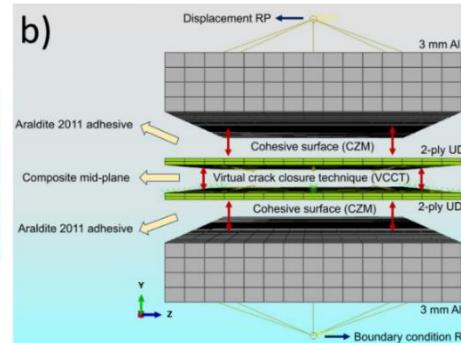
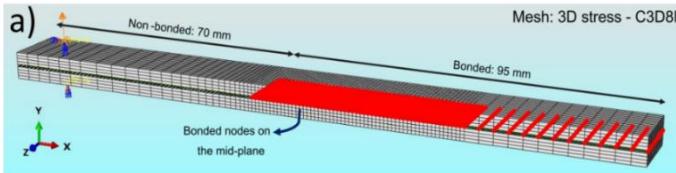
$$G_{II} = \frac{P^2}{2} \frac{\left(b_1 + b_2 + d_1 \frac{h_1}{2} - d_2 \frac{h_2}{2} \right)^2}{a_1 + a_2 + b_1 h_1 - b_2 h_2 + d_1 \frac{h_1^2}{4} + d_2 \frac{h_2^2}{4}} a^2$$

$$G = \frac{P^2}{2} [c_1 + c_2 + (d_1 + d_2)a^2]$$

These **data-reduction equations** are function of:

- The **applied load**
- The **geometry** of the specimen (sublamine thicknesses, crack length)
- The **material properties** (engineering constants and coefficients of thermal and moisture expansion)

Experimental data reduction



	FE, undesired failure	FE, perfect bond
$G_{Ic,ini}$ (kJ/m ²)	2.140	2.110
$G_{IIc,ini}$ (kJ/m ²)	0.009	0.001
$G_{IIIc,ini}$ (kJ/m ²)	0.0002	0.0002



Pure mode I and insignificant contribution of cohesive failure of the adhesive on the mid-plane ERR

